

**CAPABILITIES OF ELECTROCHEMICAL DIMENSIONAL MACHINING OF
THIN-WALLED OVERSIZED AIRCRAFT DETAILS USING ROTATING
CATHODE-INSTRUMENT**

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This article presents the results of experimental studies of electrochemical dimensional machining model sample in the form of thin-walled hemispherical shell. The studies were carried out using a specially designed and manufactured laboratory installation for local electrochemical machining of details using rotating electrode-instrument. The article presents the main units of used installation for research and the methods of used experiments are decrypted. In this case varying factors during carrying out a series of experiments were composition of electrolyte, electrolyte temperature and also current density. The studies were conducted using as electrolyte an aqueous solution of sodium hydroxide, and also an aqueous solution of ammonium nitrate.

When used as an electrolyte 15 % water solution of sodium hydroxide at a rotation speed of the electrode-instrument 20 rpm, at a current density $2\text{--}5\text{ A/cm}^2$, temperature of electrolyte $30\text{--}40\text{ }^{\circ}\text{C}$ it has been found alignment of the sample surface through the thickness in the radial axes, moreover, the thickness extreme deviations are negligible. Using 15 % of aqueous solution of ammonium nitrate as a main component and 2.5 % of ammonium citrate as a complexing agent does not allow to achieve the desired results. During the analysis of the results extreme deviations in thickness in the radial direction amounted from ± 0.05 to $\pm 0.09\text{ mm}$ when removing 0.1 mm of metal. Non-uniformity of metal removal was detected in the axial direction.

Thus, it is established, that for carrying out electrochemical machining process of thin-walled oversized details of responsible appointment, which are applied in the aerospace industry, an aqueous solution of sodium hydroxide is most expedient to use as an electrolyte.

The main feature of the proposed process is its controllability, efficiency and reducing the environmental impact on the ecological conditions due to lower temperature of used electrolyte and lower concentration of electrolyte.

Keywords: *electrochemical machining, aluminium alloy, electrolyte, chemical milling.*

Вестник СибГАУ
Том 18, № 1. С. 227–231**ВОЗМОЖНОСТИ ПРИМЕНЕНИЯ ЭЛЕКТРОХИМИЧЕСКОЙ РАЗМЕРНОЙ
ОБРАБОТКИ ВРАЩАЮЩИМСЯ КАТОДОМ-ИНСТРУМЕНТОМ
ДЛЯ ДЕТАЛЕЙ ЛЕТАТЕЛЬНЫХ АППАРАТОВ**

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Представлены результаты экспериментальных исследований электрохимической размерной обработки модельных образцов в виде тонкостенной оболочки в форме полусферы. Исследования проводились с использованием специально спроектированной и изготовленной лабораторной установки для осуществления локальной электрохимической обработки деталей вращающимся электродом-инструментом. Представлены основные узлы используемой для исследований установки и приведено описание применяемой методики проведения экспериментов. При этом варьируемыми факторами в ходе проведения серии экспериментов являлись состав, температура электролита и плотность тока. Исследования проводились с использованием в качестве электролитов водного раствора гидроксида натрия, а также водного раствора азотно-кислого аммония.

При использовании в качестве электролита 15 % водного раствора гидроксида натрия при скорости вращения электрода-инструмента 20 об/мин, плотности тока $2\text{--}5\text{ A/cm}^2$, температуре $30\text{--}40\text{ }^{\circ}\text{C}$ было обнаружено выравнивание поверхности образца по толщине по радиальным осям, причём предельные отклонения по толщине незначительны. Применение 15 % водного раствора азотно-кислого аммония в качестве основного

компонента и 2,5 % лимонно-кислого аммония в качестве комплексообразователя не позволяет достичь требуемых результатов. В ходе анализа полученных результатов предельные отклонения по толщине в радиальном направлении составили от $\pm 0,05$ до $\pm 0,09$ мм при съеме 0,1 мм. Была обнаружена неравномерность съема металла в осевом направлении.

Таким образом, установлено, что для проведения процесса электрохимической обработки тонкостенных крупноразмерных деталей ответственного назначения, которые применяются в космической промышленности, наиболее целесообразно применять в качестве электролита водный раствор гидроксида натрия.

Особенностью предлагаемого процесса является его управляемость, экономичность и снижение экологической нагрузки на окружающую среду вследствие снижения температуры используемого электролита и меньшей концентрации электролита.

Ключевые слова: электрохимическая обработка, алюминиевый сплав, электролит, химическое фрезерование.

Introduction. One of the most important tasks of modern space engineering is the development and creation of new parts manufacturing technologies providing reliability, durability and safety in the operation of aircrafts. By their quality satisfy more stringent requirements than those required in other engineering industries. It should be noted that the constructions of responsible assignment used in the aerospace industry should have given technological characteristics, be resistant to the effects of space factors, safe, accessible under the price.

In these conditions it is becoming particularly urgent problem of processing large-size thin-walled details which are made of materials having specific properties. Such materials include aluminium alloys $AlCu_6Mn$, $Al-Mg-Sc$, $AlMg_6$, $AlMg_3$. Machining parts of assembly units made of aluminum alloys, using existing methods significantly complicated.

Machining thin-walled constructions of these alloys by mechanical means is not always possible, since the mechanical machining in this case is very laborious. Also details of responsible appointment for space industry should have a high surface quality ($R_a = 2.5 \mu m$) to obtain the desired level of mechanical properties [1], that is not always cost-effective using mechanical machining. This is due to the fact that the required thickness of the wall detail is very small (about 2 mm). Furthermore mechanical machining of thin-walled parts can adversely affect the final mechanical properties of the finished product.

One way of solving this problem is the use of chemical milling. However, this process has a number of significant shortcomings. For example, for use chemical milling of large parts to require large expenses for reagents and materials as the machining method, as the machined surface area is greater than $10 m^2$. It should also be noted a significant duration of the preparatory process for the etching of parts. High temperature of alkaline solution (up to $90^\circ C$) has a negative impact on the environment and health of personnel. Furthermore, the chemical milling process is out of control, so machining is carried out periodically with a drain solution and control of wall thickness that does not provide the required accuracy.

Thus, it is advisable to research, development and application of modern methods of machining large-sized thin-walled parts of aircrafts. Such methods include electrochemical dimensional machining (ECDM) [2].

Application of electrochemical dimensional machining. ECDM is a complex set of interrelated processes, control of which is a challenge in technical terms,

consists in the necessity of stabilization a large number of process parameters [3; 4]. This method is based on electrochemical dissolution of the detail metal at high electrical current densities. The point of ECDM method is that some parts of the detail anodic dissolves in the flowing electrolyte at high speed. The use of high current densities allows machining process at high speed. ECDM significant advantages compared to other methods is the ability machining all metals and alloys, regardless of their properties [5–12]. Furthermore, the used electrode-instrument in this tool does not wear out, which can significantly reduce material costs and reduce the complexity of manufacturing parts [13; 14], and machining does not entail metal structure change.

Based on previous studies [15] regimes of ECDM are determined for aluminium alloy $AlCu_6Mn$, which make it possible to provide the necessary surface roughness ($R_a = 2.5 \mu m$) and high precision machining. Research ECDM regimes of large parts that having the form bodies of rotation and made of alloy $AlMg_6$ carried out at laboratory unit [16], which scheme is shown in fig. 1.

Description of laboratory unit for ECDM. Laboratory unit includes a sample model 1, which is mounted on a stand 7, source of power 3, potentiometer 6.

Model sample represented thin shell (4 mm), made of alloy $AlMg_6$, и having the shape of a hemisphere with an inner diameter 490 mm. At the same time on the outside unimproved surface of the model sample points are plotted to control the wall thickness. Control is carried out in the axial and radial direction. 6 control points deposited at each of 8 generatrix. Numbering is carried from the periphery to the center of rotation of cathode-instrument (fig. 2).

Moreover, the original wall thickness of the processed sample controlled with thickness gage at every point. Assemble and install the power supply connections, recording devices. The electrolyte is poured into the sample model to a fixed level. During processing, the voltage and temperature of the electrolyte controlled. After processing the electrolyte is drained, model sample washed, wall thickness measured, wherein received data recorded.

The methodology of experiments and analysis of the results. In the first case for machining the model sample used 15 % water solution $NaOH$ at a rotation speed of electrode-instrument 2 rpm, current density $2-5 A/cm^2$, temperature $30-40^\circ C$. Electrolyte temperature was maintained using a flow cooling the outer surface of the test sample.

Studies have shown that during electrochemical machining of aluminum alloy surface of the sample thickness is equalized along radial axes (fig. 3). Extreme deviation in thickness when removing 1 mm is ± 0.11 mm, when removing 2 mm – ± 0.095 mm. In the axial direction

when removing 1 mm there are no significant changes in extreme deviations of thickness. With an increase removing to 2 mm there is an increase extreme deviations in thickness to ± 0.37 mm.

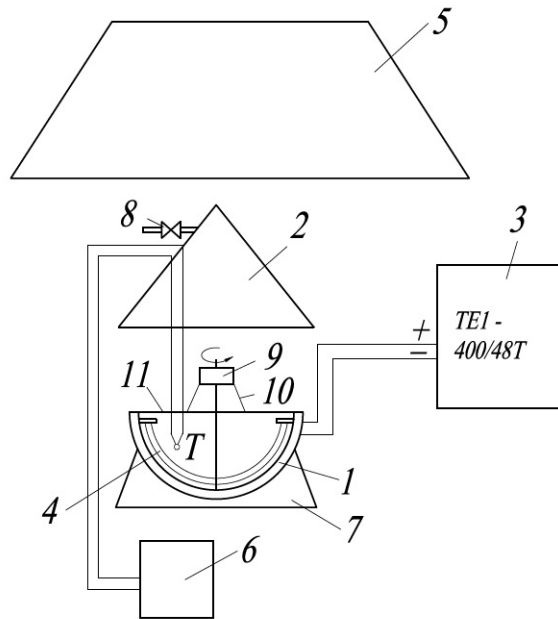


Fig. 1. Scheme of laboratory installation ECDM:
1 – model sample; 2 – bell for taking gas samples; 3 – source of power; 4 – cathode-instrument; 5 – dry box; 6 – potentiometer; 7 – stand for model sample; 8 – sampling valve; 9 – electric motor; 10 – bracket; 11 – cross-piece

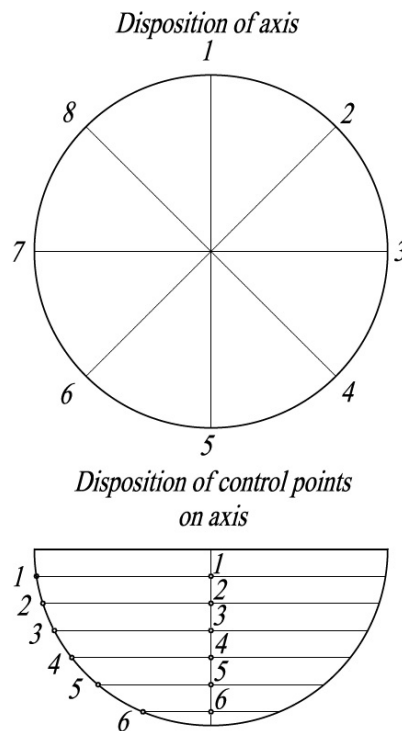


Fig. 2. Disposition scheme of control points on the model sample

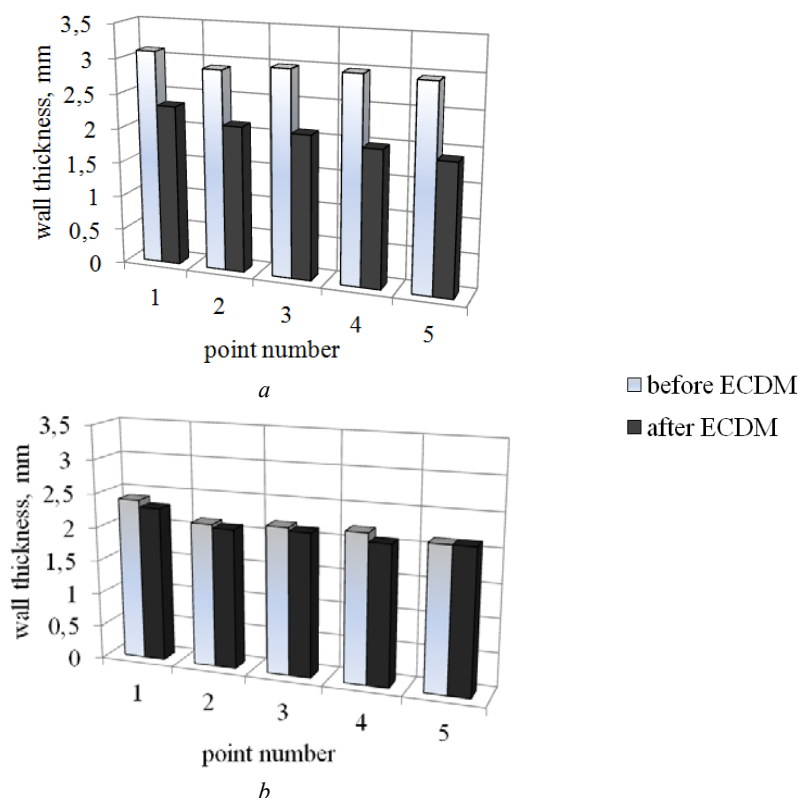


Fig. 3. Changes in the wall thickness during ECDM in the solutions 15 % NaOH (a) and 15 % NH_4NO_3 + 2.5 % $\text{C}_5\text{H}_{11}\text{O}_7\text{N}$ (b)

In the second case, the electrolyte used in which included 15 % water solution NH_4NO_3 as a main component and 2.5 % ammonium dihydrogen citrate as complexing agent. The rotation speed of the electrode-instrument was 2 rpm at a current density 12 A/cm^2 , temperature $30\text{--}60^\circ\text{C}$.

Extreme deviations in thickness in the radial direction amounted from ± 0.05 to ± 0.09 mm when removing 0.1 mm. In the axial direction there are large extreme deviations in thickness (from ± 0.21 to ± 0.36 mm when removing 0.1 mm), that indicates about uneven of metal removal. The results can be attributed that processing time in the central part of the sample is much larger than at the periphery, as the speed of the electrode-instrument increases from the periphery to the center (from 0.01 m/s to 0.06 m/s).

As can be seen from the diagram shown in fig. 3, ECDM of the detail using as the electrolyte 15 % of water solution NaOH gives the best results. Wall thickness of the details is reduced uniformly.

When using the solution of 15 % NH_4NO_3 + 2.5 % $\text{C}_5\text{H}_{11}\text{O}_7\text{N}$ there is minimum amount of removal. Furthermore, in some areas there is no metal dissolution, which leads to uneven of metal removal.

Conclusion. During the analysis of the results following can be concluded:

1. Basic scheme of the installation for the machining of the model sample have been developed.
2. Designed and manufactured installation that allows machining the model sample in the form of hemisphere with inner diameter 490 mm.
3. As the electrolyte appropriate to apply 15 % solution of NaOH with temperature $30\text{--}40^\circ\text{C}$.
4. The current density at ECDM should be $2\text{--}5 \text{ A/cm}^2$, which makes it possible machining large parts with an

area of machined surface more than 10 m^2 using a rotating cathode-instrument.

5. With increasing distance from the center of the workpiece machining speed reduced, as it decreases the time finding of electrode-instrument over a point on the periphery. To avoid this need to use a cathode-instrument with a variable width of the working surface with increasing width of the electrode-instrument from the center towards the periphery 6 times, because the linear speed of rotation of the cathode from the center to the periphery is changed by 6 times.

6. ECDM process of large parts of aircrafts performed locally due to the impossibility of processing large area (more than 10 m^2). Simultaneous machining the entire surface of the part would require significant energy costs, since the amperage required for the ECDM process, would have been more 300'000 A, which is not practicable in an industrial environment.

7. It is possible to make the ECDM process controllable by changing the amperage, the temperature of the electrolyte solution and applying a sectional electrode-instrument.

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