

**SIDE GROUNDED CONDUCTORS DIPPED IN A SUBSTRATE OF A MICROSTRIP LINE,
AS A TOOL OF LINE CHARACTERISTICS CONTROL**

I. Ye. Sagieva*, T. R. Gazizov

Tomsk State University of Control Systems and Radioelectronics

40, Lenina Av., Tomsk, 634050, Russian Federation

*E-mail: indira_sagieva@mail.ru

Electrical design of on-board radio-electronic equipment is an important stage in spacecraft design. High characteristics of printed circuit boards (PCBs) are essential for miniature units that have reliability, speed, stability of electrophysical parameters, electromagnetic compatibility. In order to do that, new design and technological solutions are necessary, in particular transmission lines with stable characteristics of per-unit-length delay (τ) and wave impedance (Z). One of the main lines, realized on a PCB is a microstrip line (MSL). In multi-layer PCBs it is often used with polygons. However, their influence on the stability of characteristics is investigated insufficiently.

The purpose of the work is to investigate the dependence of τ and Z of MSL on the distance between the side grounded conductors as they are dipped in a substrate.

*In the TALGAT software we built a geometric model of the line cross-section and calculated (using the method of moments) the matrices (3*3) of per-unit-length coefficients of electrostatic induction taking into account the dielectric as well as ignoring it. We calculated the values for the change of distance between side conductors (s), dipped in a substrate, for different values of the height of the side conductors ($h1$). We revealed that for large values of s (unlike small ones), approaching of the side conductors to the air-substrate boundary does not increase but it decreases the value of τ . When $s = 0.38$ mm, the change of the value of $h1$ in the whole range almost doesn't change the values of τ and, therefore zero sensitivity of τ to changes of $h1$ is possible. Thus we can obtain the required Z value in the range from 48 to 59 Ohms by changing the value of $h1$.*

These results are obtained for particular values of the parameters of the line. However it is easy to obtain similar dependencies for other values of parameters. The results can be used to design transmission lines with stable delay under control of the impedance value.

Keywords: printed circuit board, microstrip line, per-unit-length delay, impedance, polygons, zero sensitivity.

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**БОКОВЫЕ ЗАЗЕМЛЕННЫЕ ПРОВОДНИКИ, УГЛУБЛЕННЫЕ В ПОДЛОЖКУ
МИКРОПОЛОСКОВОЙ ЛИНИИ, КАК СРЕДСТВО КОНТРОЛЯ ЕЁ ХАРАКТЕРИСТИК**

И. Е. Сагиева*, Т. Р. Газизов

Томский государственный университет систем управления и радиоэлектроники

Российская Федерация, 634050, г. Томск, просп. Ленина, 40

*E-mail: indira_sagieva@mail.ru

Электрическое проектирование бортовой радиоэлектронной аппаратуры является важным этапом создания космических аппаратов. Высокие характеристики печатных плат (ПП) важны для миниатюрных узлов, обладающих надежностью, быстродействием, стабильностью электрофизическими параметров, электромагнитной совместимостью. Для этого необходимы новые конструкторско-технологические решения, в частности, линии передачи со стабильными характеристиками погонной задержки (τ) и волнового сопротивления (Z). Одной из основных линий, реализуемых на ПП, является микрополосковая линия (МПЛ). В многослойных ПП она часто используется с полYGONами. Однако их влияние на стабильность характеристик мало исследовано.

Цель статьи – исследовать зависимости τ и Z МПЛ от расстояния между боковыми заземленными проводниками при их углублении в подложку.

*В системе TALGAT построена геометрическая модель поперечного сечения линии и методом моментов вычислены матрицы (порядка 3*3) погонных коэффициентов электростатической индукции с учетом диэлектрика и без него. Выполнены вычисления при изменении расстояния между боковыми проводниками (s), углубленными в подложку, для разных значений высоты боковых проводников ($h1$). Выявлено, что при больших значениях s , в отличие от малых, приближение боковых проводников к границе «воздух–подложка» не увеличивает, а уменьшает значения τ . При $s = 0,38$ мм изменение значения $h1$ во всем диапазоне почти не меняет значения τ , а значит, возможна нулевая чувствительность τ к изменению $h1$. При этом изменением значения $h1$ можно получить требуемое значение Z в диапазоне от 48 до 59 Ом.*

Данные результаты получены для конкретных значений параметров линии. Однако легко получить аналогичные зависимости при других значениях параметров. Результаты работы могут быть использованы для проектирования линий передачи со стабильным значением задержки при контроле волнового сопротивления.

Ключевые слова: печатная плата, микрополосковая линия, погонная задержка, волновое сопротивление, полигоны, нулевая чувствительность.

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Introduction. Electrical design of on-board radio-electronic equipment is an important stage in the space-craft design [1]. High characteristics of printed circuit boards (PCBs) are important for miniature units [2; 3] that have reliability [4], speed, stability of electrophysical parameters [5], electromagnetic compatibility [6]. In order to do that, new design and technological solutions are necessary, in particular transmission lines with stable characteristics of per-unit-length delay (τ) and wave impedance (Z). Thus the research of these characteristics is relevant [7–10].

One of the main lines, realized on PCB is MSL. Various modifications of MSL are the most interesting, for example, suspended and inverted strip lines which make it possible to obtain zero sensitivity of the per-unit-length delay and wave impedance to the change in the thickness of dielectric layers [11]. A similar pattern was found in MSL coated with a grounded conductor, shielded MSL [12] and MSL with side grounded conductors placed above [13]. There is a detailed analysis of modifications and variances in such a line and its varieties. Multilayer PCBs use a variety of MSL, for example, MSL with polygons on different layers that allows to obtain a stable value of the per-unit-length delay [14]. Meanwhile, it is useful to study the characteristics of MSL with side conductors grounded only on one layer located near the boundary of two environments.

The purpose of the work is to investigate the dependence of τ and Z of MSL on the distance between the side grounded conductors as they are dipped in a substrate.

To achieve the objective, we investigated the structure of MSL with side conductors dipped in the substrate (fig. 1). We chose the following cross-sectional parameters (they are close to typical): the width of the signal conductor is $w = 0.3$ mm, the thickness of the signal and side grounded conductors is $t = 18 \mu\text{m}$, the width of the side conductors is $w_1 = 1$ mm, the thickness of the dielectric substrate is $h = 1$ mm, the relative permittivity of the substrate is $\epsilon_r = 4.5$.

Line modeling. In the TALGAT [15] software we built the geometric model of the line cross-section and calculated (using the method of moments) the matrices (3*3) of per-unit-length coefficients of electrostatic induction taking into account the dielectric as well as ignoring it.

From the matrices we took the values (hereinafter C and C_0) of the diagonal element corresponding to the signal conductor and calculated the values of τ and Z (v_0 is the speed of light in vacuum):

$$\tau = (C/C_0)^{0.5} / v_0, \quad Z = 1/(v_0(CC_0)^{0.5}).$$

We calculated the values for change of distance between the side conductors s , dipped in a substrate, for the height of the side conductors $h_1 = 0.1\text{--}0.9$ mm (fig. 2). Fig. 2 shows that when s increases, the value of τ decreases smoothly, and Z increases. At small values of h_1 , the changes of τ and Z are small, but the growth of h_1 leads to an increase in the value of τ and a decrease in the value of Z , and at small values of s the changes of τ and Z are more significant.

Approaching of the side conductors to the air-substrate boundary has a special effect on the characteristics being studied. Therefore, we performed simulation with a smaller step at the air-substrate boundary: at $h_1 = 0.8; 0.82; 0.84; 0.86; 0.88; 0.9$ mm (fig. 3). The analysis of fig. 3 shows a similar behavior of dependencies, but it reveals its specificity as well. It is expressed in the amplification of the influence of the side conductors when they approach the air-substrate boundary for small values of s . When $s = 0.1$ mm, the value of τ increases from 5.56 to 5.82 ns/m. We noticed that for large values of s , approaching of the side conductors to the air-substrate boundary does not increase but it decreases the values of τ . When $s = 0.6$ mm this decrease is maximal and is from 5.33 ns/m to 5.29 ns/m. When $s = 0.38$ mm, the change of the value of h_1 in the whole range almost doesn't change the values of τ and, therefore zero sensitivity of τ to changes of h_1 is possible. Thus we can obtain the required Z value in the range from 48 to 59 Ohms by changing the value of h_1 .

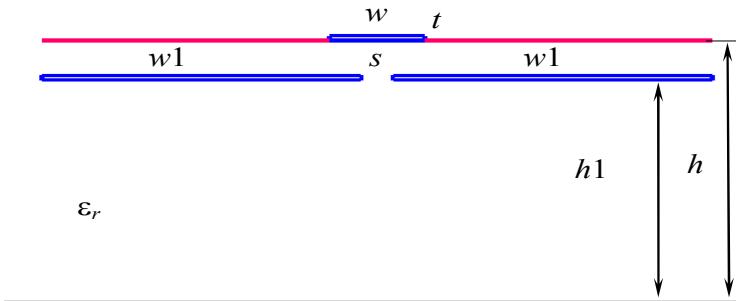
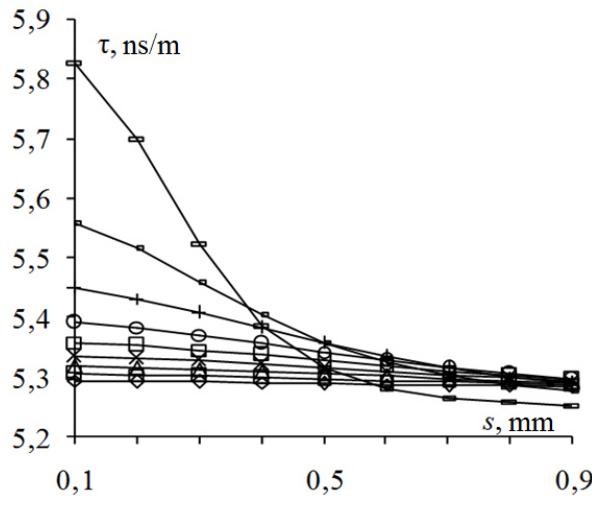
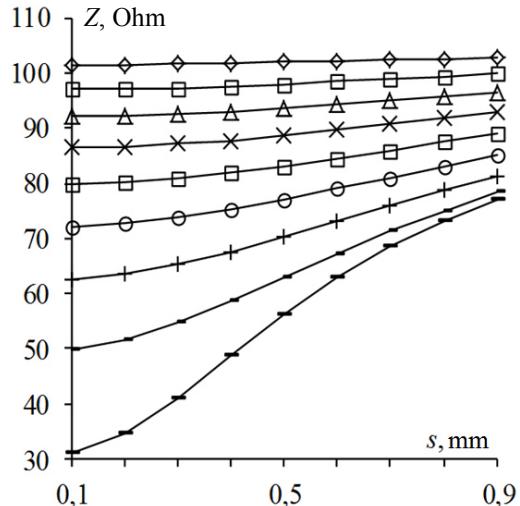


Fig. 1. Cross-section of MSL with side grounded conductors, dipped in a substrate

Рис. 1. Поперечное сечение МПЛ с боковыми заземленными проводниками, углубленными в подложку



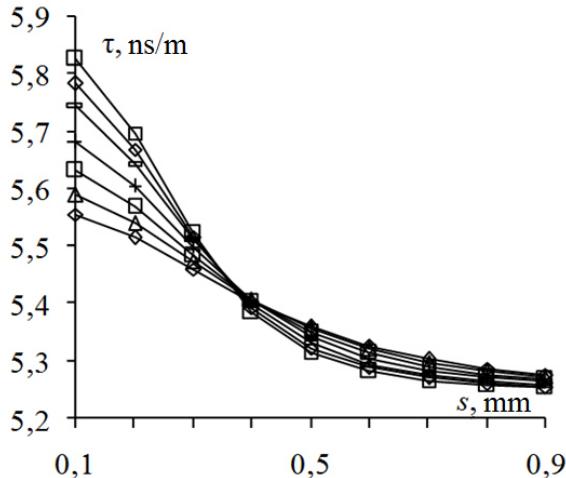
a



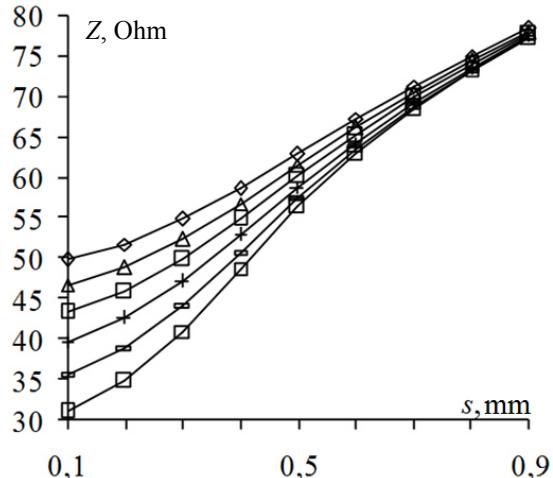
b

Fig. 2. Dependences of τ (a) and Z (b) on s
at $h_1 = 0.1 (\diamond); 0.2 (\square); 0.3 (\Delta); 0.4 (\times); 0.5 (\square); 0.6 (\circ); 0.7 (+); 0.8 (-); 0.9 (-)$ mm

Рис. 2. Зависимости τ (а) и Z (б) от s
при $h_1 = 0.1 (\diamond); 0.2 (\square); 0.3 (\Delta); 0.4 (\times); 0.5 (\square); 0.6 (\circ); 0.7 (+); 0.8 (-); 0.9 (-)$ мм



a



b

Fig. 3. Dependences of (a) and Z (b) on s
at $h_1 = 0.8 (\diamond); 0.82 (\Delta); 0.84 (\square); 0.86 (+); 0.88 (-); 0.9 (\square)$ mm

Рис. 3. Зависимости τ (а) и Z (б) от s
при $h_1 = 0.8 (\diamond); 0.82 (\Delta); 0.84 (\square); 0.86 (+); 0.88 (-); 0.9 (\square)$ мм

Conclusion. We modeled MSL with side grounded conductors dipped in a substrate. We calculated the dependence of the per-unit-length delay and the wave impedance on the distance between the grounded conductors when the depth changes. We found out that zero sensitivity of per-unit-length delay to depth changes is possible

while obtaining the required wave impedance. These results are obtained for the particular values of line parameters.

However it is easy to obtain similar dependencies for other values of parameters. The results can be used to design transmission lines with stable characteristics.

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References

1. Kochura S. G., Maksimov I. A., Maslov E. P., Pervuhin A. V. [Studying the impact of electromagnetic radiation on spacecraft with permeable instrument unit]. *Tekhnologii elektromagnitnoy sovmestimosti*. 2017, No. 3(62), P. 3–10 (In Russ.).
2. Gazizov T. R., Zabolockij A. M., Orlov P. E. [The influence of the length and the number of coils on the delay of a microstrip line]. *Infokommunikacionnye tehnologii*. 2014, Vol. 13, No. 4, P. 93–96 (In Russ.).
3. Surovcev R. S. [Impulse signal propagation in a meander line with heterogeneous dielectric filling without deformation by cross coupling]. *Doklady TUSURa*. 2014, No. 4(34), P. 34–38 (In Russ.).
4. Orlov P., Gazizov T., Zabolotsky A. Comparative electromagnetic and quasi-static simulations of a short-pulse propagation along microstrip meander delay lines with design constraints. *Journal of ELECTRICAL ENGINEERING*. 2016, Vol. 67, No. 5, P. 387–389. DOI: 10.1515/jee-2016-0056.
5. Gazizov R. R., Zabolockij A. M., Gazizov T. T. [Studying volts peak of ultra short signal impulse in a meander line in the case of the change of its geometric parameters]. *Tekhnologii elektromagnitnoy sovmestimosti*. 2016, No. 3(58), P. 11–17 (In Russ.).
6. Surovcev R. S., Gazizov T. R. [Evaluating signal integrity in printed circuit boards of autonomous navigation systems of spacecraft]. *Trudy MAI*. 2015, No. 83 (In Russ.). Available at: <https://www.mai.ru/science/trudy/published.php?ID=62204>.
7. Hamood M. K. Line thickness for various characteristic impedance of microstrip line. *Tikrit Journal of Pure Science*. 2013, Vol. 18, No. 3, P. 140–144.
8. Akhunov R. R., Kuksenko S. P., Gazizov T. R. Acceleration of Multiple Iterative Solution of Linear Algebraic Systems in Computing the Capacitance of a Microstrip Line in Wide Ranges of Its Sizes. *Journal of mathematical sciences*. 2015, Vol. 207, No. 5, P. 686–692.
9. Surovtsev R. S., Kuksenko S. P., Gazizov T. R. Analytic Evaluation of the Computational Costs for Solving Systems of Linear Algebraic Equations in Multiple Computing of the Capacitance Matrix in a Range of the Dielectric Permittivity of Dielectrics. *Journal of mathematical sciences*. 2015, Vol. 207, No. 5, P. 795–802.
10. Gazizov T. R., Kuksenko S. P., Akhunov R. R. Acceleration of Multiple Solution of Linear Systems for Analyses of Microstrip Structures. *International journal of mathematical models and methods in applied sciences*. 2015, Vol. 9, P. 721–726.
11. Gazizov T. R. [Characteristics of suspended strip line and reversed strip line]. *Izvestiya vuzov. Fizika*. 1996, Vol. 39, No. 2, P. 126–128 (In Russ.).
12. Sagiyeva I. [Studying characteristics of shielded microstrip line]. *Izvestiya vuzov. Fizika*. 2017, Vol. 60, No. 12/2, P. 103–107 (In Russ.).
13. Sagiyeva I. Ye. [Modeling characteristics of a microstrip line with side grounded conductors]. *Materialy XIII mezhdunarodnoy nauchno-prakticheskoy konferentsii "Elektronnye sredstva i sistemy upravleniya", posvyashchennaya 55-letiyu TUSURA* [Materials of the XIII International Scientific and Practical Conference "Electronic Tools and Control Systems", dedicated to the 55th anniversary of TUSUR,]. Tomsk, November 29 – December 1, 2017, Part 2, P. 19–20 (In Russ.).
14. Gazizov T. R., Salov V. K., Kuksenko S. P. Stable delay of microstrip line with side grounded conductors. *Wireless Communications and Mobile Computing*. 2017, Vol. 2017, 5 p. DOI:10.1155/2017/1965739.
15. Kuksenko S. P., Zabolotskiy A. M., Melkozerov A. O., Gazizov T. R. [New capacities of the system of modeling electromagnetic compatibility]. *Doklady TUSURa*. 2015, No. 2 (36), P. 45–50 (In Russ.).

Библиографические ссылки

1. Исследование воздействия электромагнитного излучения на космический аппарат с негерметичным приборным отсеком / С. Г. Kochura [и др.] // Технологии электромагнитной совместимости. 2017. № 3(62). С. 3–10.
2. Газизов Т. Р., Заболоцкий А. М., Орлов П. Е. Влияние длины и количества витков на задержку микрополосковой линии // Инфокоммуникационные технологии. 2014. Т. 13, № 4. С. 93–96.
3. Распространение импульса в меандровой линии с неоднородным диэлектрическим заполнением без искажений его формы перекрестными наводками / Р. С. Суровцев [и др.] // Доклады ТУСУРа. 2014. № 4(34). С. 34–38.
4. Orlov P., Gazizov T., Zabolotsky A. Comparative electromagnetic and quasi-static simulations of a short-pulse propagation along microstrip meander delay lines with design constraints // Journal of ELECTRICAL ENGINEERING. 2016. Vol. 67, no. 5. P. 387–389. DOI: 10.1515/jee-2016-0056.
5. Газизов Р. Р., Заболоцкий А. М., Газизов Т. Т. Исследование максимума напряжения сверхкороткого импульса в микрополосковой меандровой линии при изменении ее геометрических параметров // Технологии электромагнитной совместимости. 2016. № 3(58). С. 11–17.
6. Суровцев Р. С., Газизов Т. Р. Оценка целостности сигналов в печатных платах системы автономной навигации космического аппарата [Электронный ресурс] // Труды МАИ. 2015. № 83. URL: <https://www.mai.ru/science/trudy/published.php?ID=62204> (дата обращения: 5.10.2015).
7. Hamood M. K. Line thickness for various characteristic impedance of microstrip line // Tikrit Journal of Pure Science. 2013. Vol. 18, No. 3. P. 140–144.
8. Akhunov R. R., Kuksenko S. P., Gazizov T. R. Acceleration of Multiple Iterative Solution of Linear Algebraic Systems in Computing the Capacitance of a Microstrip Line in Wide Ranges of Its Sizes // Journal

- of mathematical sciences. 2015. Vol. 207, № 5. P. 686–692.
9. Surovtsev R. S., Kuksenko S. P., Gazizov T. R. Analytic Evaluation of the Computational Costs for Solving Systems of Linear Algebraic Equations in Multiple Computing of the Capacitance Matrix in a Range of the Dielectric Permittivity of Dielectrics // Journal of mathematical sciences, 2015. Vol. 207, № 5. P. 795–802.
10. Gazizov T. R., Kuksenko S. P., Akhunov R. R. Acceleration of Multiple Solution of Linear Systems for Analyses of Microstrip Structures // International journal of mathematical models and methods in applied sciences. 2015. Vol. 9. P. 721–726.
11. Газизов Т. Р. Характеристики подвешенной и обращенной полосковых линий // Известия вузов. Физика. 1996. Т. 39, № 2. С. 126–128.
12. Сагиева И. Исследование характеристик экранированной микрополосковой линии // Известия вузов. Физика. 2017. Т. 60, № 12/2. С. 103–107.
13. Сагиева И. Е. Моделирование характеристик микрополосковой линии с боковыми заземленными проводниками сверху // Электронные средства и системы управления : материалы XIII Междунар. науч.-практ. конф., посвященной 55-летию ТУСУРа (29 нояб.–1 дек. 2017, г. Томск). Томск, 2017. Ч. 2. С. 19–20.
14. Gazizov T. R., Salov V. K., Kuksenko S. P. Stable delay of microstrip line with side grounded conductors // Wireless Communications and Mobile Computing. 2017. Vol. 2017, Article ID 1965739. 5 p. DOI: 10.1155/2017/1965739.
15. Новые возможности системы моделирования электромагнитной совместимости TALGAT / С. П. Куксенко [и др.] // Докл. Том. гос. ун-та систем управления и радиоэлектроники. 2015. № 2(36). С. 45–50.

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