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EXTERNAL BOUNDARIES OF POLE LOCALIZATION REGION FORMULATION FOR TRANSFER FUNCTION WITH INTERVAL-GIVEN PARAMETERS

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In this paper the approach for external boundary of pole localization region formulation for transfer function with interval-given parameters is proposed. The boundary is formulated as analytic piecewise function of characteristic polynomial parameters of the given transfer function.

Analytic formulation of external boundary of poles localization region allows to reduce computations since existing methods require iterative numeric calculations of characteristic equation roots with fixed step size for edges mapping or full interval root locus mapping as well. Formulated boundary allows to clearly describe system behavior and calculate variation ranges of performance indexes. In addition, piecewise function that constrains gives new opportunities for parametric controller synthesis for systems introduced by transfer functions with interval-given parameters.

The results can find its practical application in aerospace engineering problems of mathematical analysis and synthesis for highly-precise systems of self-direction missiles.

In the research the boundary formulation is performed for third order transfer function. Transfer function order was chosen due to the fact that many physical systems and objects can be described mathematically with the third order transfer function, e.g. model of missile target-seeking head with gyro stabilized drive is described with this model.

The research was performed on the basis of the following step sequence: firstly, analytical solving of cubic equation applying Cardano's formula; secondly, interval root locus edges functions obtaining, next external vertexes set obtaining and, finally, external border formulation and plotting.

Key words: system analysis, root locus, interval systems, poles localization.

ПОСТРОЕНИЕ ВНЕШНЕЙ ГРАНИЦЫ ОБЛАСТИ ЛОКАЛИЗАЦИИ ПОЛЮСОВ ПЕРЕДАТОЧНОЙ ФУНКЦИИ С ИНТЕРВАЛЬНО-ЗАДАННЫМИ ПАРАМЕТРАМИ

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Предлагается подход к построению внешней границы области локализации полюсов передаточной функции с интервально-заданными параметрами. Граница области локализации полюсов формируется как аналитическая кусочно-заданная функция зависимости от параметров характеристического полинома заданной передаточной функции.

Аналитическое построение внешней границы области локализации полюсов позволяет сокращать объем вычислений, так как существующие подходы требуют итеративного численного нахождения корней характеристического уравнения для полного отображения корней с заданным шагом или для построения ребер на корневой плоскости. Наличие границы области локализации позволяет однозначно охарактеризовать поведение системы, в том числе вычислить диапазоны изменения значений корневых показателей качества.

Кроме того, наличие аналитической кусочно-заданной функции, определяющей область локализации полюсов на корневой плоскости, открывает дополнительные возможности в решении задач параметрического синтеза регуляторов для систем автоматического управления, представленных передаточными функциями с интервально-заданными параметрами.

Практическая значимость полученных результатов может быть достигнута в аэрокосмической промышленности, в частности, при решении задач анализа и синтеза в высокоточных системах ракетного самонаве-

дения, построения их математических моделей, с целью извлечения экономического эффекта, связанного с количеством натурных экспериментов.

В представленной работе построение границы области локализации полюсов осуществляется для передаточной функции третьего порядка. Порядок передаточной функции выбран исходя из того, что на практике, множество объектов и систем могут быть описаны такой моделью. Например, модель ракетной головки самонаведения с гиростабилизированным приводом описывается передаточной функцией третьего порядка.

В основе предлагаемого подхода лежит следующая последовательность действий: аналитическое решение кубического уравнения, получаемого по формуле Кардано, получение функциональных зависимостей для ребер многопараметрического корневого годографа, формирование набора внешних вершин корневого годографа, построение кусочно-заданных функций для внешних границ области локализации полюсов.

Ключевые слова: анализ систем, корневой годограф, интервальные системы, локализация полюсов.

Introduction. In classical automatic control theory, parameters of technological objects models and control systems are expressed in real fixed values, but in practice the exact parameter values and coefficients are unknown and can be represented as some tolerance interval values of a given parameter.

Referring to a number of works devoted to the study of systems with interval-given parameters [1–9], it can be noted that the boundaries of the pole localization region of the transfer function (TF) of these systems are obtained by calculating the roots of the characteristic equation at some discrete step of varied parameter changing, i.e. numerical construction of boundaries takes place. This approach allows to determine numerical values of root quality indicators for a given class of systems with some given accuracy and similarly to evaluate the stability of the system as a whole. However, it requires a lot of iterative calculations. In turn, when solving the problems of the regulator parametric synthesis, the absence of analytical dependence does not provide accurate understanding of how the changing values of parameters affect the quality indicators.

The above problems of synthesis and system analysis with interval-given parameters require analytical description.

Task Setting. The task for the third-order TF with interval-given parameters to obtain the analytical function describing the external region of pole localization at any parameter values within the specified intervals.

Obtaining basic dependencies. Let us assume that given is some 3rd order TF system with characteristic polynomial of

$$\Delta(s) = a_3 s^3 + a_2 s^2 + a_1 s + a_0. \quad (1)$$

Edges of root locus are formed by motion of polynomial roots (1) under changing value of one or several polynomial coefficients.

It is known that the roots of the cubic equation can be analytically found applying Cardano's formula. Cardano's formula gives solution to the following cubic equation

$$y^3 + py + q = 0. \quad (2)$$

To bring the original characteristic equation of the system (1) to the appearance (2), we obtain a set of coefficients of the equation

$$b_{n-j+1} = \frac{a_{j-1}}{a_n}, j = \overline{1, n},$$

where n – order of the system characteristic polynomial (1). Values p and q will respectively equal

$$p = -\frac{b_1^2}{3} + b_2,$$

$$q = \frac{2b_1^3}{27} - \frac{b_1 b_2}{3} + b_3.$$

We will then substitute the obtained values p and q into Cardano's formula

$$y = \sqrt[3]{-\frac{q}{2} + \sqrt{\frac{q^2}{4} + \frac{p^3}{27}}} + \sqrt[3]{-\frac{q}{2} - \sqrt{\frac{q^2}{4} + \frac{p^3}{27}}}..$$

$$\text{With regard to substitution } s = y - \frac{a_2}{3a_3} [10]$$

$$s_{1,2,3}(a_3, a_2, a_1, a_0) = \begin{cases} \left(u(a_3, a_2, a_1, a_0) + v(a_3, a_2, a_1, a_0) \right) - \frac{a_2}{3a_3}, \\ \left(u(a_3, a_2, a_1, a_0) e_2 + v(a_3, a_2, a_1, a_0) e_1 \right) - \frac{a_2}{3a_3}, \\ \left(u(a_3, a_2, a_1, a_0) e_1 + v(a_3, a_2, a_1, a_0) e_2 \right) - \frac{a_2}{3a_3}, \end{cases} \quad (3)$$

where

$$u(a_3, a_2, a_1, a_0) = \begin{cases} \frac{9a_3 a_2 a_1 - 27a_0 a_3^2 - 2a_2^3}{54a_3^3} + \\ + \sqrt{\left(27a_0 a_3^2 - 9a_3 a_2 a_1 + 2a_2^3 \right)^2 + 4\left(3a_1 - a_2^2 \right)^3} \end{cases} \quad (4)$$

$$v(a_3, a_2, a_1, a_0) = \begin{cases} \frac{9a_3 a_2 a_1 - 27a_0 a_3^2 - 2a_2^3}{54a_3^3} - \\ - \sqrt{\left(27a_0 a_3^2 - 9a_3 a_2 a_1 + 2a_2^3 \right)^2 + 4\left(3a_1 - a_2^2 \right)^3} \end{cases} \quad (5)$$

$$\begin{aligned} e_1 &= -\frac{1}{2} + i \frac{\sqrt{3}}{2}, \\ e_2 &= -\frac{1}{2} - i \frac{\sqrt{3}}{2}. \end{aligned} \quad (6)$$

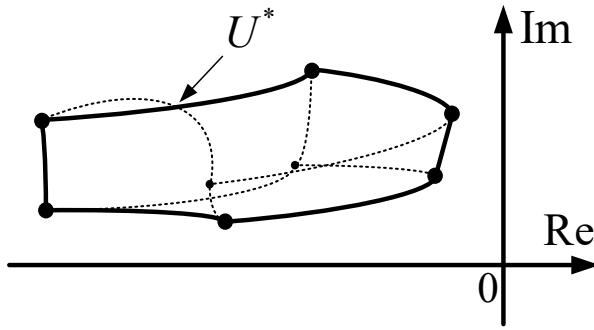


Fig. 1 Interval Root Locus with internal and external edges intersection

Рис. 1. Корневой годограф системы с наличием взаимного пересечения внешнего и внутреннего ребер

Using the property $e_1^2 = e_2$ и $e_2^2 = e_1$, the expression for the roots of the equation can be rewritten as

$$\begin{aligned} s(a_3, a_2, a_1, a_0) = & \\ = & \left(u(a_3, a_2, a_1, a_0) e_1^k + v(a_3, a_2, a_1, a_0) e_2^k \right) - \frac{a_2}{3a_3}, \\ k = & \{0, 1, 2\}. \end{aligned} \quad (7)$$

In addition, the pole configuration will be determined by the discriminant equation value (2), the expression for which is

$$Q = \frac{q^2}{4} + \frac{p^3}{27}.$$

Let us consider the case of $Q \in (0; +\infty)$, which correlates with the pair of complex-conjugate poles and one real pole.

For a system with interval-given parameters, the edge of a multi-parameter root locus (MPRL) is formed by changing the value of one of interval parameters at fixed boundary values of other parameters. Thus, the analytical expression E_f^{kl} for the MPRL edge when changing parameter values a_i can be determined according to (3) as

$$E_f^{kl} = s_k(a_l), k = \overline{1, n}, l = \overline{1, m} \quad (8)$$

where n – order of characteristic polynomial, m – number of interval parameters.

Given that the presented expressions are obtained with respect to the coefficients at the degrees of characteristic equation, it is also fair to use dependency data for more complex types of uncertainties. For affine, polylinear, and polynomial uncertainties, coefficients at degrees in general form can be represented as $a_k = \phi(q_1, q_2, \dots, q_l)$ [11] and are further substituted into (8), having the following appearance

$$E_f^{kl} = s_k(\phi(q_l)), k = \overline{1, n}, l = \overline{1, m}.$$

Description of system pole boundary regions localization under the interval type of uncertainty. So-called external vertices must be selected to form the ex-

ternal boundary of the TF system pole localization region with the parametric uncertainty of the interval type. The procedure for determining the membership of an MPRL vertex in a set of external vertices is based on the values of the departure angles. The angle of the edge departs from the vertex is defined as

$$\Theta = 180^\circ - \sum \Theta_k + \sum \Theta_l, \quad (9)$$

Under parameter increase, or

$$\Theta = -\sum \Theta_k + \sum \Theta_l \quad (10)$$

under decrease [12–13], where Θ_k and Θ_l – angles between real axis and vectors, directed from the pole under study to neighbor poles and zeros respectively. The vertex will be referred to as external vertex in case all of its exit angles lie within the sector in 180° [14].

It should be noted that when considering TF systems with interval-given parameters of the third order and higher, edge intersection connecting two external vertices and the edge connecting one external vertex with an internal vertex are possible, as shown in fig. 1.

Edges intersection is possible in case they come out of the same vertex and are formed by changing the values of the coefficients at degrees i, j for which the condition $|i - j| \geq 3$ is met. For the coefficients under study with indexes i, j the following equation system can be formulated

$$\begin{cases} \sin((j-i)\varphi) = 0; \\ \sum_z a_z |s|^{j+z} \sin((z-j)\varphi) = 0; \end{cases} \quad (11)$$

where i, j – the indices of vertex polynomial parameters which variation forms intersecting edges, z are the set of indices of the remaining coefficients of the vertex polynomial. Considering the part of the MPRL formed only by poles with a positive imaginary part, the angle φ will be defined by the expression

$$\varphi = \pi - \frac{\pi}{|i-j|}, |i-j| = 3, 4, 5, \dots \quad (12)$$

Substituting φ into the second expression (11), we obtain $|s|$. Knowing the module and argument, we will find the actual value of the edges intersection point U^* . However, to correctly create the system of analytical expressions defining the boundary of localization region of a given system, we must define parametric coordinates of the point U^* , i. e. interval parameter values a_i, a_j , under which the edges, coming out from the boundary vertex, created by the movement of these parameters possess a common point [15].

Numerical parameter values a_i^*, a_j^* in point U^* may be obtained from equations

$$\begin{cases} s_2(a_i, a_2, a_1, a_0) = U^*; \\ s_2(a_3, a_2, a_1, a_j) = U^*; \end{cases} \quad (13)$$

where a_i, a_j – changeable parameters, a_2, a_3 – fixed border values of corresponding parameters.

Example. Let us consider the system described by the 3-order TF with interval-given parameters and characteristic polynomial of

$$\Delta(s) = [a_3]s^3 + [a_2]s^2 + [a_1]s + [a_0],$$

Having obtained a set of external vertices, a set of variable parameters forming the edges connecting the external vertices, and having determined the presence and further coordinates of the specific point of edges intersection, we can form a system of analytical expressions defining the borders of the pole system location region (fig. 3)

$$F(a_3, a_2, a_1, a_0) = \begin{cases} f_1(a_1) = u(\underline{a}_3, \overline{a}_2, a_1, \underline{a}_0)e_2^k + v(\underline{a}_3, \overline{a}_2, a_1, \underline{a}_0)e_1^k - \frac{\overline{a}_2}{3\underline{a}_3}, a_1 \in [\underline{a}_1; \overline{a}_1]; \\ f_2(a_2) = u(\underline{a}_3, a_2, \overline{a}_1, \underline{a}_0)e_2^k + v(\underline{a}_3, a_2, \overline{a}_1, \underline{a}_0)e_1^k - \frac{\overline{a}_2}{3\underline{a}_3}, a_2 \in [\underline{a}_2; \overline{a}_2]; \\ f_3(a_0) = u(\underline{a}_3, a_2, \overline{a}_1, a_0)e_2^k + v(\underline{a}_3, a_2, \overline{a}_1, a_0)e_1^k - \frac{\overline{a}_2}{3\underline{a}_3}, a_0 \in [\underline{a}_0; \overline{a}_0]; \\ f_4(a_3) = u(a_3, \underline{a}_2, \overline{a}_1, \overline{a}_0)e_2^k + v(a_3, \underline{a}_2, \overline{a}_1, \overline{a}_0)e_1^k - \frac{\overline{a}_2}{3\underline{a}_3}, a_3 \in [\underline{a}_3; \overline{a}_3]; \\ f_5(a_1) = u(\overline{a}_3, \underline{a}_2, a_1, \overline{a}_0)e_2^k + v(\overline{a}_3, \underline{a}_2, a_1, \overline{a}_0)e_1^k - \frac{\overline{a}_2}{3\underline{a}_3}, a_1 \in [\underline{a}_1; \overline{a}_1]; \\ f_6(a_2) = u(\overline{a}_3, a_2, \overline{a}_1, \overline{a}_0)e_2^k + v(\overline{a}_3, a_2, \overline{a}_1, \overline{a}_0)e_1^k - \frac{\overline{a}_2}{3\underline{a}_3}, a_2 \in [\underline{a}_2; \overline{a}_2]; \\ f_7(a_0) = u(\overline{a}_3, \overline{a}_2, \overline{a}_1, a_0)e_2^k + v(\overline{a}_3, \overline{a}_2, \overline{a}_1, a_0)e_1^k - \frac{\overline{a}_2}{3\underline{a}_3}, a_0 \in [\underline{a}_0; \overline{a}_0]; \\ f_8(a_3) = u(a_3, \overline{a}_2, \underline{a}_1, \overline{a}_0)e_2^k + v(a_3, \overline{a}_2, \underline{a}_1, \overline{a}_0)e_1^k - \frac{\overline{a}_2}{3\underline{a}_3}, a_3 \in [\underline{a}_3^*; \overline{a}_3]; \\ f_9(a_0) = u(\underline{a}_3, \overline{a}_2, \underline{a}_1, a_0)e_2^k + v(\underline{a}_3, \overline{a}_2, \underline{a}_1, a_0)e_1^k - \frac{\overline{a}_2}{3\underline{a}_3}, a_0 \in [\underline{a}_0^*; \overline{a}_0]. \end{cases} \quad (14)$$

where $a_3 = [0.7; 0.9]$, $a_2 = [1.7; 2.2]$, $a_1 = [5.2; 7.6]$, $a_0 = [2.5; 3.7]$.

Let us numerically build MPRL for a given system (fig. 2). Since MPRL is symmetrical to the real axis, only the part with a positive imaginary part is considered. Applying (9) and (10), we will define a set of external vertexes of the given system root locus. The obtained set of external vertexes makes the route: $5 \rightarrow 7 \rightarrow 3 \rightarrow 4 \rightarrow 12 \rightarrow 10 \rightarrow 14 \rightarrow 13 \rightarrow 5$, with external boundary of transition $13 \rightarrow 5$ created by the part of the transition $13 \rightarrow 5$ and $5 \rightarrow 6$. For this system the edge $5 \rightarrow 6$ is formed via polynomial root $P_{5 \rightarrow 6}(s) = \underline{a}_3 s^3 + \overline{a}_2 s^2 + \underline{a}_1 s + \underline{a}_0$, with the edge $13 \rightarrow 5$ root transition $P_{13 \rightarrow 5}(s) = [\underline{a}_3] s^3 + \overline{a}_2 s^2 + \underline{a}_1 s + \underline{a}_0$. Indexes of the given edges coefficients differ by 3, which is a must requirement for intersection. Therefore, the index of variable parameter of one edge is $i = 3$, of the other is $j = 0$. Substituting the obtained values into (11) and (12), we obtain $\varphi = \frac{2\pi}{3}$, $|s| = 2.3636$. Applying Euler's formula, we will receive the point of intersection $U^* = -1.1818 + 2.047i$. Solving (13), we obtain $a_3^* = 0.7415$ and $a_0^* = 3.047$.

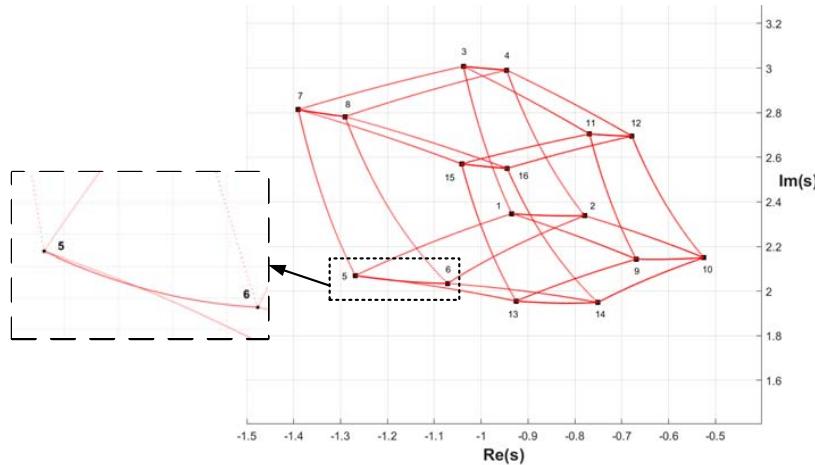


Fig. 2 Interval Root Locus for the given system

Рис. 2. Корневой годограф заданной системы

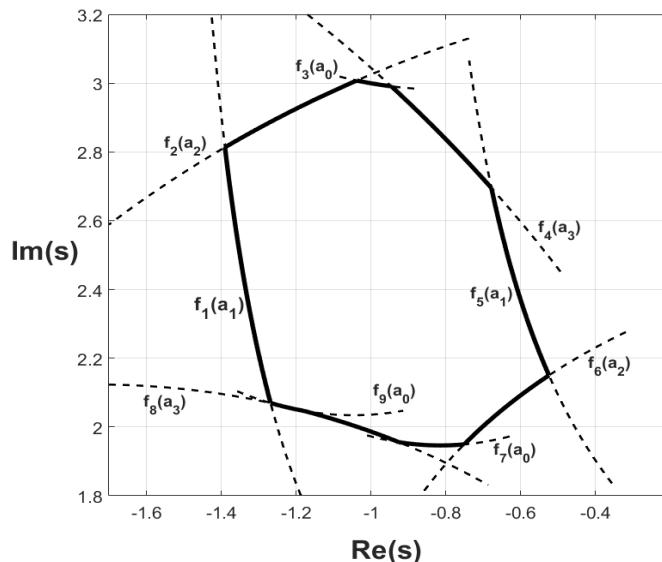


Fig. 3. Piecewise function $F(a_3, a_2, a_1, a_0)$ forming the external boundary of poles localization region

Рис. 3. Кусочно-заданная функция $F(a_3, a_2, a_1, a_0)$, образующая внешнюю границу области локализации полюсов ПФ системы

Conclusion. The work justified a need for analytical approach to the study of systems with interval-given parameters. The analytical approach allows to obtain a clear idea of the system behavior, as well as formalize the synthesis procedure. According to the results of the study, analytical expressions for edges were worked out, a piecewise function for the boundary of the pole localization region of the 3-order transfer function with interval-given parameters was obtained. Furthermore, a numerical example was considered, the results of which confirm the above-mentioned theoretical research.

References

1. Ezangina T. A., Gayvoronskiy S. A., Efimov S. V. Construction of Interval Polynomial Ensure the Specified Degree of Robust Stability. 2014 CACS International

Automatic Control Conference (CACS 2014), Taiwan, 2014, P. 292–295.

2. Gayvoronskiy S. A., Ezangina T. A., Pushkarev M. I. The interval-parametric synthesis of a linear controller based on the coefficient parameters of robust stability and oscillation. 15th International conference on Sciences and Techniques of Automatic Control & computer engineering – STA'2014. Tunisia, 2014, P. 754–757.

3. Polyak B. T., Scherbakov P. S. Robastnaya ustoychivost' i upravlenie [Robust Stability and Control]. Moscow, Nauka Publ., 2002, 303 p.

4. Jolen L., Kiefer M., Didrit O., Walter E. Applied Interval Analysis. Springer-Verlag London, 2001, 468 p.

5. Ross Barmish B. New Tools for robustness of linear systems. Macmillan Publishing Company New York, 1994, 394 p.

6. Zhmud V., Zavorin A. The Design of the Control System for Object with Delay and Interval-Given Parameters. *2015 International Siberian Conference on Control and Communications (SIBCON)*. Russia, 2015, P. 1–6.
7. Weinmann A. Uncertain Models and Robust Control. Springer-Verlag Wien GmbH, 1991, 722 p.
8. Ackermann J. Robust Control. The parameter Space Approach 2nd ed. Springer-Verlag London, 2002, 483 p.
9. Yi-Wei Tu, Ming-Tzu Ho. Robust low-order controller synthesis for model matching of interval plants and its application to servo motor control. *18th IEEE International Conference on Control Applications Part of 2009 IEEE Multi-conference on Systems and Control*. Russia, 2009, P. 968–973.
10. Korn G. A., Korn T. A. Mathematical Handbook for scientists and engineers. Definitions, theorems and formulas for reference and review. Second, enlarged and revised edition. McGraw-Hill Book Company, 1968, 720 p.
11. Bhattacharyya S. P., Chapellat H. Robust control: the parametric approach. L.H. Keel – Prentice Hall, 1995.
12. Barmish B. R., Tempo R. The robust root locus. *Automatica*. 1990, Vol. 26, B2, P. 283–292.
13. Uderman E. G. *Metod kornevogo godografa v teorii avtomatycheskikh system* [The root hodograph method in the theory of automatic systems]. Moscow, Nauka Publ., 1972, 448 p.
14. Sukhodoev M. S., Gayvoronskiy S. A., Zamyatin S. V. [Analysis and synthesis of robust automatic control systems in Matlab]. *Izvestiya Tomskogo politekhnicheskogo universiteta*. 2008, Vol. 312, No. 5, P. 61–65 (In Russ.).
15. Sukhodoev M. S. *Kornevoy analiz i sintez sistem interval'nymi parametrami na osnove vershinnykh kharakteristicheskikh polinomov. Kand. Diss.* [Root analysis and synthesis of systems with interval parameters based on vertex characteristic polynomials. Cand. Diss.]. Tomsk, 2008.
- Библиографические ссылки**
1. Ezangina T. A., Gayvoronskiy S. A., Efimov S. V. Construction of Interval Polynomial Ensure the Specified Degree of Robust Stability // 2014 CACS International Automatic Control Conference (CACS 2014). Taiwan, 2014. P. 292–295.
 2. Gayvoronskiy S. A., Ezangina T. A., Pushkarev M. I. The interval-parametric synthesis of a linear controller based on the coefficient parameters of robust stability and oscillation // 15th International conference on Sciences and Techniques of Automatic Control & computer engineering – STA'2014. Tunisia, 2014. P. 754–757.
 3. Поляк Б. Т., Щербаков П. С. Робастная устойчивость и управление. М. : Наука, 2002. 303 с.
 4. Applied Interval Analysis / L. Jolen, M. Kiefer, O. Didrit et al. London : Springer-Verlag, 2001. 468 p.
 5. Ross Barmish B. New Tools for robustness of linear systems. New York : Macmillan Publishing Company, 1994. 394 p.
 6. Zhmud V., Zavorin A. The Design of the Control System for Object with Delay and Interval-Given Parameters // 2015 International Siberian Conference on Control and Communications (SIBCON). Russia, 2015. P. 1–6.
 7. Weinmann A. Uncertain Models and Robust Control. Springer-Verlag Wien GmbH, 1991. 722 p.
 8. Ackermann J. Robust Control. The parameter Space Approach 2nd ed. London : Springer-Verlag, 2002. 483 p.
 9. Yi-Wei Tu, Ming-Tzu Ho. Robust low-order controller synthesis for model matching of interval plants and its application to servo motor control // 18th IEEE International Conference on Control Applications Part of 2009 IEEE Multi-conference on Systems and Control. Russia, 2009. P. 968–973.
 10. Korn G. A., Korn T. A. Mathematical Handbook for scientists and engineers. Definitions, theorems and formulas for reference and review. Second, enlarged and revised edition. McGraw-Hill Book Company, 1968. 720 p.
 11. Bhattacharyya S. P., Chapellat H., Keel L. H. Robust control: the parametric approach. Prentice Hall, 1995.
 12. Barmish B. R., Tempo R. The robust root locus // *Automatica*. 1990. Vol. 26, B2. P. 283–292.
 13. Удерман Э. Г. Метод корневого годографа в теории автоматических систем. М. : Наука, 1972. 448 с.
 14. Суходоеv M. C., Гайворонский С. А., Замятин С. В. Анализ и синтез робастных систем автоматического управления в среде Matlab // Известия Томского политех. ун-та, 2008. Т. 312, № 5. С. 61–65.
 15. Суходоеv M. C. Корневой анализ и синтез систем с интервальными параметрами на основе вершинных характеристических полиномов : дис. канд. техн. наук : 05.13.01. Томск, 2008.

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