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Методика выбора материала оснастки для изготовления элементов конструкции летательных аппаратов

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Развитие современных материалов и технологий изготовления элементов конструкций летательных аппаратов из полимерных композиций требует обоснования выбора технологической оснастки. Основными критериями выбора материала технологической оснастки являются физико-технические характеристики материала, обеспечение требуемых точностей изготовления оснастки, а также экономическая целесообразность. Выбор материала оснастки зависит от технологии изготовления элементов конструкции из полимерных композиционных материалов. В работе представлена методика выбора материала оснастки для изготовления деталей методом вакуумной инфузии. Представлены результаты сравнительного анализа типовых материалов оснастки, используемых в производстве. Показано, что основными критериями при проведении сопоставительного анализа являются: температура эксплуатации, стойкость к воздействию растворителей, устойчивость к механическим воздействиям; ремонтопригодность; значение коэффициента линейного температурного расширения (КЛТР); стабильность геометрии оснастки и ее герметичность. Результаты сопоставительного анализа показали, что для изготовления оснастки, при использовании в технологическом процессе высоких температур, наиболее целесообразными являются металлы и углепластики. В работе представлен алгоритм выбора материала оснастки для изготовления деталей из полимерных композиционных материалов. Отмечено, что при изготовлении элементов конструкции на основе стеклопластика и углепластика материал оснастки следует выбирать такой же, что и у детали. Это позволяет, во-первых, обеспечить одинаковые КЛТР, что важно при горячем формовании детали, а, во-вторых, устранить коробление детали в процессе ее остывания на оснастке. Однако достижение заданных точностей такой оснастки требует учета обработки оснастки гелькоутом после ее изготовления. В работе приведен подход к количественной оценке экономической целесообразности выбора материала оснастки. Показано, что только совокупность технических, технологических и экономических факторов позволяет обосновать целесообразность используемого материала оснастки для конкретного производства элементов конструкции летательного аппарата.

Ключевые слова: инфузия, материал оснастки, элементы конструкции летательного аппарата.

Rigging material selection methodology for aircraft elements design

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The development of modern materials and technologies for manufacturing structural elements of aircraft from polymer compositions requires justification for the choice of technological rigging. The physical and technical characteristics of the material, ensuring the required accuracy of rigging manufacturing, as well as economic feasibility are the main criteria for choosing the material of technological rigging. The main criteria for choosing a rigging material are the physical and technical characteristics of the material, ensuring the required accuracy of rigging manufacturing, as well as economic feasibility. The choice of rigging material depends on the technology for manufacturing structural elements from polymer composite materials. The paper presents a methodology for selecting rigging material for manufacturing details using the vacuum infusion method. The method of rigging materials selection for aircraft construction elements production from polymer composition by vacuum infusion is considered in the paper. The results of a comparative analysis of typical rigging materials used in production are presented. It is shown that the main criteria for a comparative analysis are: temperature, resistance to solvents, resistance to mechanical stress; maintainability; the value of the coefficient of linear thermal expansion; the stability of the geometry of the rigging and its tightness. The results of the comparative analysis showed that metals and carbon fiber are the most appropriate for the manufacture of rigging, when using high temperatures in the technological process. The paper presents an algorithm for choosing the rigging material for manufacturing the details from polymer composite materials. It is noted that in the manufacture of structural elements based on fiberglass and carbon fiber, the rigging material should be chosen the same as that of the detail. This allows, firstly, to ensure the same CLTE, what is important when hot detail formation, and, secondly, to eliminate the warping of the detail during its cooling on the rigging. However, achieving the specified accuracy of such rigging requires taking into account the processing of the rigging with a gelcoat after its manufacture. The paper presents an approach to quantifying the economic feasibility of the choice of rigging material. It is shown that only a combination of technical, technological and economic factors makes it possible to justify the expediency of the rigging material used for the specific production of aircraft structural elements.

Keywords: infusion, rigging material, aircraft structural elements.

Introduction

Infusion technology has become widely used in the manufacture of structural elements of aircraft (AC) from polymer composite materials (PCM) [1-5]. Moreover, this technology is used for the manufacture of both a power set of aircraft (frames, small frames) [6], and for the manufacture of aircraft skinings and even interiors [2; 7]. This method of manufacturing the elements of aircraft structures allows to ensure the smallest number of defects (voids, pores) in the layers of PCM at a relatively low cost of technological equipment [1; 4; 5]. Increasing requirements to the accuracy of manufacturing details from PCM, the use of new PCM components (resins, woven and non-woven materials), as well as economic aspects, for example, in terms of the serialisation of products, require a revision of the methodology for selecting rigging materials when using infusion technology. Currently used rigging materials have different physical and technical characteristics. For example, riggings made from medium-density fiberboard (MDF) have good processability, but poor resistance to external factors (temperature, humidity, etc.). Rigging made of metals, for example, duralumin, have mirror-like characteristics: they are more difficult for processing, but are resistant to external influences [8-10].

Currently, there are no clear methodological recommendations for choosing rigging materials, taking into account economic feasibility and their physical and technical characteristics. When manufacturing the serial products, the impact of the cost of rigging is reduced depending on the increase in the volume of products manufactured on it [11; 12]. However, at the same time, the wearing of the equipment increases, what can result in a significant decrease in the accuracy of the aircraft's structural elements. The purpose of this article is to develop a methodology for selecting rigging material for the manufacture of aircraft structural elements using the vacuum method infusion.

Research methodology

The choice of rigging material involves formalizing the criteria by which such a choice will be made. The main, practically important, criteria are: operating temperature, resistance to solvents, resistance to mechanical influences; maintainability; value of the coefficient of linear thermal expansion (CLTE); stability of the rigging geometry and its tightness [1, 13, 14]. The choice of these criteria is based, inter alia, on the following considerations.

Operating temperature of the rigging. The temperature conditions for the manufacture of aircraft structural elements using the vacuum infusion method are determined by the types of resins used and their polymerization technologies [1; 3; 4]. For example, when manufacturing products using the TO200 epoxy binder (TU 2257-055-59846689-2016, «Itekma» LLC, Russia), heating is carried out to 180 °C to polymerize the resin. In this case, the material of the rigging must not only withstand this temperature and not undergo destruction, but also maintain its shape with the given accuracy.

Chemical resistance. The rigging should not be damaged by solvents or specialized release agents. The rigging should be easily cleaned from resin residues and release agents using solvents recommended for resins.

Resistance to mechanical stress and maintainability. The rigging must be resistant to external mechanical influences. Moreover, the material of the rigging must allow repairing of the working surface in case of damage, for example, abrasion or chipping during its operation.

The requirement to a low CLTE value is due to the use of high-temperature polymerization processes of the finished product blanks. Moreover, the CLTE of the rigging material should be close to the CLTE of the polymer composite material of the product. It should be noted that taking into account the expansion of the rigging during the heating process does not guarantee the absence of warping of the part after molding [15].

Tightness. Vacuuming of a prepared product blank during its manufacture using the vacuum infusion method requires high tightness of the rigging material. The presence of pores in the rigging material can lead to the defects (bubbles, pores) in the final product.

Results and their discussion

The comparative analysis of commonly used rigging materials is presented in the table.

The following designations are used: «+» – the criterion is met; «±» – the criterion is partially met; «-» – the criterion is not met; k is the maximum number of details that can be manufactured on this rigging, taking into account its wear. The cost of rigging manufacturing is given relative to rigging made from MDF with dimensions 2×2×2 m.

The analysis of the materials available on the market for the manufacture of rigging shows that when using high temperatures in the technological process, metals and carbon fiber are the most appropriate. The algorithm for selecting rigging material for manufacturing aircraft structural elements from PCM using the vacuum infusion method is presented in Fig. 1.

Comparative analysis of rigging materials

	MDF	Model plastic	Duralumin (D16T)	Alloy Invar	Glass-plastic	Carbon fiber
Temperature resistance	-	±	+	+	-	+
Solvent resistance	±	±	+	+	±	±
Resistance to mechanical stress	-	-	±	+	±	±
Maintainability	±	+	±	±	+	+
CLTE	±	-	-	+	±	+
Geometry stability	-	±	+	+	±	±
Tightness	-	±	+	+	±	±
Present cost of rigging manufacturing (<i>E</i>)	1,0	2,5±0,3	10,0±1,0	20,0±2,0	7,0±0,7	10,0±1,0
<i>k</i>	1	3	200	300	70	100

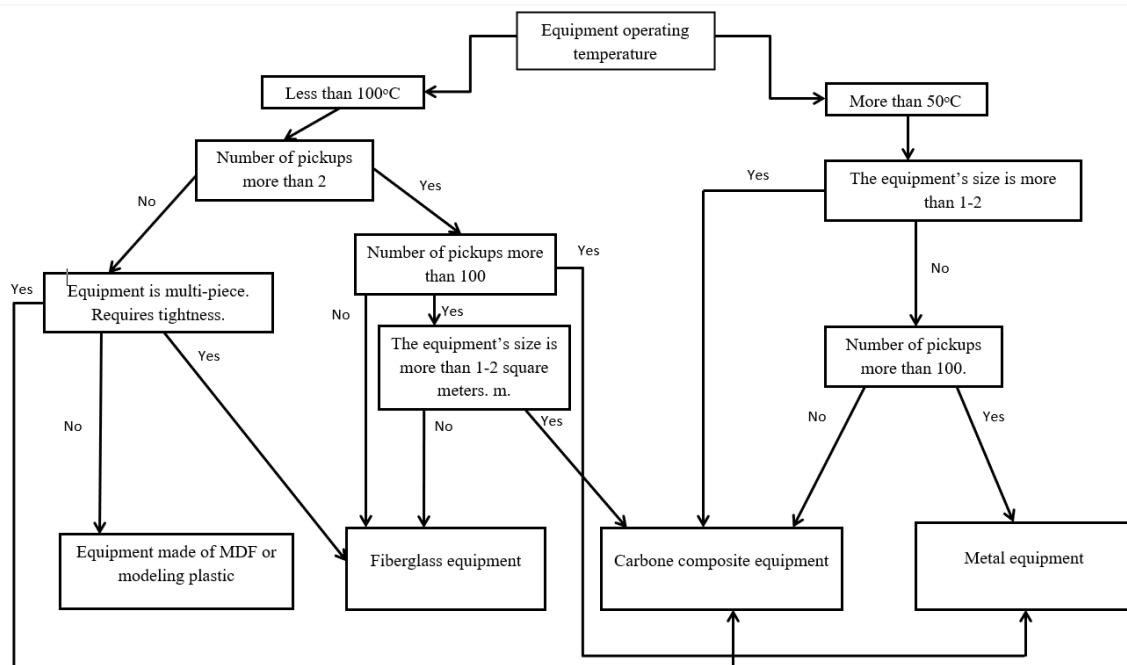


Рис. 1. Алгоритм выбора материала оснастки для изготовления элементов конструкции ЛА из ПКМ

Fig. 1. The algorithm for selecting the rigging material for the manufacture of aircraft structural elements from PCM

Nevertheless, it should be noted that the use of model plastic as a rigging material is promising. In fact, model plastic is a polymer composite material with dispersed filling. Polyurethanes of various brands are usually used as a binder in this material. By choosing the filler, its concentration, as well as the grade of polyurethane, it is possible to provide characteristics that meet the specified requirements of the technological process. Currently, the market presents mainly foreign brands of model plastic,

which do not always meet production requirements. For example, a significant CLTE compared to carbon fiber and the presence of open cells (pores) (see the table) require additional costs for the manufacture of technological rigging. An example of manufacturing of rigging from model plastic is shown in Fig. 2

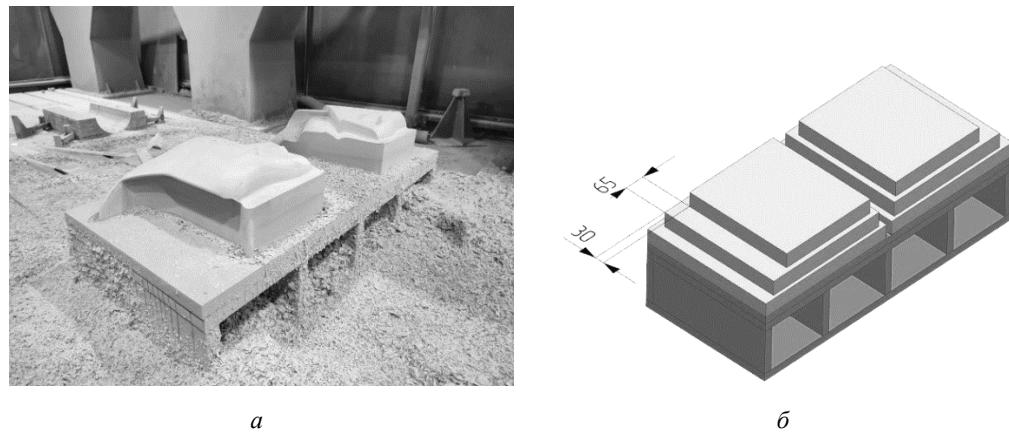


Рис. 2. Изготовление оснастки из модельного пластика:

a – заготовка мастер-модели на станке с ЧПУ; *б* – заготовка для изготовления мастер-модели из модельного пластика на каркасе из МДФ

Fig. 2. Production of rigging from model plastic:

a – blank of the master model on a NPC machine; *b* – blank for the production of a master model from model plastic on an MDF frame

Separately, it should be noted that when manufacturing structural elements from fiberglass and carbon fiber, the rigging material should be chosen the same as that of the detail. This allows, firstly, to ensure the same CLTE, what is important when thermoforming a detail, and secondly, to eliminate warping of the detail during its cooling on the rigging. However, even in this case it is not always possible to ensure high accuracy of the specified dimensions of the details. For example, this may be due to the use of a «gelcoat» in the structure of such rigging, as opposed to the master model on which it is located (Fig. 3).



Рис. 3. Оснастка из углепластика

Fig. 3. Carbon fiber composite rigging

This, in turn, increases the requirements to the accuracy of rigging manufacturing, and, consequently, an increase in its cost should be expected.

Assessing the economic feasibility when choosing the material of the rigging, it is necessary to take into account not only its present value E (see the table), but also the cost (Σ) of the batch of details, manufactured using it:

$$\sum = X \cdot n + \frac{k - n + 1}{k} \cdot Y, \quad (1)$$

where X is the cost of one detail, Y is the cost of one rigging for the manufacture of such details, n is the number of details manufactured. For example, with the cost of an aircraft structural element $X = 200,000$ rubles, the cost of rigging made from model plastic $Y_{МП} = 50,000$ rubles, from carbon fiber plastic $Y_{УП} = 150,000$ rubles, the cost of a batch of details of 50 pieces will be:

$$\sum_{УП} = 10'076'500 \text{ rubles}, \quad \sum_{МП} = 10'533'333 \text{ rubles}.$$

Conclusion

The comparative analysis of rigging materials for the manufacture of details using the vacuum infusion method made it possible to formalize the methodology of the choice of the material that best satisfies the required criteria. It should be noted that only a combination of technical, technological and economic factors makes it possible to justify the feasibility of the rigging used for the specific production of aircraft structural elements.

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Библиографические ссылки

1. Особенности изготовления полимерных композиционных материалов методом вакуумной инфузии / М. И. Душин, Л. В. Чурсова, А. В. Хрульков, Д. И. Коган // Вопросы материаловедения. 2013. № 3. С. 33–40.
2. Изготовление стеклопластиковых обшивок методом вакуумной инфузии с использованием эпоксиангидридного связующего и полупроницаемой мембранны / М. М. Григорьев, А. В. Хрульков, Я. М. Гуревич, Н. Н. Панина // Тр. ВИАМ. 2014. № 2. С. 4–8.
3. Донецкий К. И., Усачева М. Н., Хрульков А. В. Методы инфузии для изготовления полимерных композиционных материалов (обзор). Ч. 1 // Труды ВИАМ. 2022. № 6. С. 58–67.
4. Методы инфузии для изготовления полимерных композиционных материалов (обзор). Ч. 2 / А. В. Хрульков, К. И. Донецкий, М. Н. Усачева, А. Н. Горянский // Тр. ВИАМ. 2022. № 7. С. 50–62.
5. Мостовые конструкции из композитов / А. Е. Ушаков, Ю. Г. Кленин, Т. Г. Сорина и др. // Композиты и наноструктуры. 2009. № 3. С. 25–37.
6. Проектирование и оптимизация технологического процесса вакуумной инфузии для изготовления кузова вагона-хоппера из полимерных композиционных материалов / А. Е. Ушаков, А. А. Сафонов, И. В. Сергеичев и др. // Проблемы машиностроения и надежности машин. 2015. № 3. С. 102–109.
7. Руденко М. С., Михеев А. Е., Гирн А. В. Технология изготовления сотовых заполнителей из полимерных композиционных материалов // Сибирский аэрокосмический журнал. 2021. Т. 22, № 2. С. 391–397.
8. Комаров В. А., Куркин Е. И., Кузнецов А. С. Исследование и модификация оснастки и формообразующей поверхности с целью повышения точности изготовления деталей методом вакуумной инфузии // Изв. Самарского науч. центра РАН. 2013. Т. 15, № 6-3. С. 710–717.

9. Янович А. Современные композитные материалы для производства оснастки // Композитный мир. 2016. № 6. С. 36–40.
10. Исследования и разработка автоклавных и безавтоклавных технологий формования ПКМ / А. В. Хрульков, М. И. Душин, Ю. О. Попов, Д. И. Коган // Авиационные материалы и технологии. 2012. № 5. С. 292–301.
11. Исследование свойств полимерного композиционного материала для изготовления пресс-форм ЛГМ / Шаршин В. Н., Кечин В. А., Сухоруков Д. В., Сухорукова Е. В., Середа Е. В. // Литейщик России. 2011. № 12. С. 40–42.
12. Дектярев А. В., Морозов В. Н. Технико-экономическое обоснование аддитивных технологий в отечественную судостроительную промышленность // Гипотеза. 2018. № 3. С. 15–24.
13. Андреев А. В., Петропольский В. С. Оптимизация выбора материала мастер–моделей для изделий из полимерных композиционных материалов в условиях единичного и опытного производства в изделиях авиационной техники // Вопросы проектирования и производства конструкций летательных аппаратов. 2015. № 2. С. 20–28.
14. Моделирование влияния оснастки на конечную форму изделий из полимерного композита / М. В. Козлов, С. В. Шешенин, И. В. Макаренко, Д. А. Белов // Вычислительная механика сплошных сред. 2016. Т. 9, № 2. С. 145–161.
15. Карташова Е. Д., Муйземнек А. Ю. Технологические дефекты полимерных слоистых композиционных материалов // Изв. вузов. Поволжский регион. Технические науки. 2017. Т. 42, № 2. С. 79–89.

References

1. Dushin M. I., Chursova L. V., Khrul'kov A. V., Kogan D. I. [Peculiarities of production of polymer composites by vacuum infusion method]. *Voprosy materialovedeniya*. 2013, No. 3, P. 33–40 (In Russ.).
2. Grigor'ev M. M., Khrul'kov A. V., Gurevich Ya. M., Panina N. N [Production of fiberglass liners by vacuum infusion using an epoxy-hydride binder and a semi-permeable membrane]. *Trudy VIAM*. 2014, No. 2, P. 4–8 (In Russ.).
3. Donetskiy K. I., Usacheva M. N., Khrul'kov A. V. [Infusion methods for the production of polymer composites (review). Part 1]. *Trudy VIAM*. 2022, No. 6, P. 58–67 (In Russ.).
4. Khrul'kov A. V., Donetskiy K. I., Usacheva M. N., Goryanskiy A. N. [Infusion methods for the manufacture of polymer composites (Review). Part 2]. *Trudy VIAM*. 2022, No. 7, P. 50–62 (In Russ.).
5. Ushakov A. E., Klenin Yu. G., Sorina T. G. et al. [Composite bridge structures]. *Kompozity i nanostruktury*. 2009, No. 3, P. 25–37 (In Russ.).
6. Ushakov A. E., Safonov A. A., Sergeichev I. V. et al. [Design and optimization of vacuum infusion process for manufacturing of hopper body made of polymer composites]. *Problemy mashinostroyeniya i nadezhnosti mashin*. 2015, No. 3, P. 102–109 (In Russ.).
7. Rudenko M. S., Mikheev A. E., Girn A. V. [Technology of honeycomb core production from polymer composites]. *Sibirskiy aerokosmicheskiy zhurnal*. 2021, Vol. 22, No. 2, P. 391–397 (In Russ.).
8. Komarov V. A., Kurkin E. I., Kuznetsov A. S. [Research and modification of rigging and forming surface in order to improve the accuracy of parts manufacturing by vacuum infusion]. *Izvestiya Samarskogo nauchnogo tsentra Rossiyskoy akademii nauk*. 2013, Vol. 15, No. 6-3, P. 710–717 (In Russ.).
9. Yanovich A. [Modern composite materials for rigging production]. *Kompozitnyy mir*. 2016, No. 6, P. 36–40 (In Russ.).
10. Khrul'kov A. V., Dushin M. I., Popov Yu. O., Kogan D. I. [Research and development of autoclave and non-autoclave technologies for PCM molding]. *Aviatsionnye materialy i tekhnologii*. 2012, No. 5, P. 292–301 (In Russ.).

11. Sharshin V. N., Kechin V. A., Sukhorukov D. V. et al. [Study of the properties of polymer composite material for the production of LGM molds]. *Liteyshchik Rossii*. 2011, No. 12, P. 40–42 (In Russ.).
12. Dektyarev A. V., Morozov V. N. [Feasibility study on the implementation of additive technologies in the domestic shipbuilding industry]. *Gipoteza*. 2018, No. 3, P. 15–24 (In Russ.).
13. Andreev A. V., Petropol'skiy V. S. [Optimization of material selection of master models for polymer composite products in the conditions of single and pilot production in the products of aeronautical engineering]. *Voprosy proektirovaniya i proizvodstva konstruktsiy letatel'nykh apparatov*. 2015, No. 2, P. 20–28 (In Russ.).
14. Kozlov M. V., Sheshenin S. V., Makarenko I. V., Belov D. A. [Modeling the influence of rigging on the final shape of polymer composite products]. *Vychislitel'naya mekhanika sploshnykh sred*. 2016, Vol. 9, No. 2, P. 145–161 (In Russ.).
15. Kartashova E. D., Muyzemnek A. Yu. [Technological defects in polymer layered composites]. *Izvestiya vysshikh uchebnykh zavedeniy. Povolzhskiy region. Tekhnicheskie nauki*. 2017, Vol. 42, No. 2, P. 79–89 (In Russ.).

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